

AMT®
Advanced Mould Technology



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cunova offers a unique combination of know-how and experience in all key technologies for the production of highperformance moulds for casting ferrous and nonferrous alloys as well as for re-melting.

The Company

cunova's corporate goal is to develop and manufacture products that meet customer demands, finding solutions for their specific applications, and providing services as a long-term partner. cunova's strategy for accomplishing this goal is based on a highly skilled and experienced workforce. cunova has the ability to invent and develop new materials and innovative production processes via ongoing advancement and training of our employees and the continual improvement of its organisational structures.



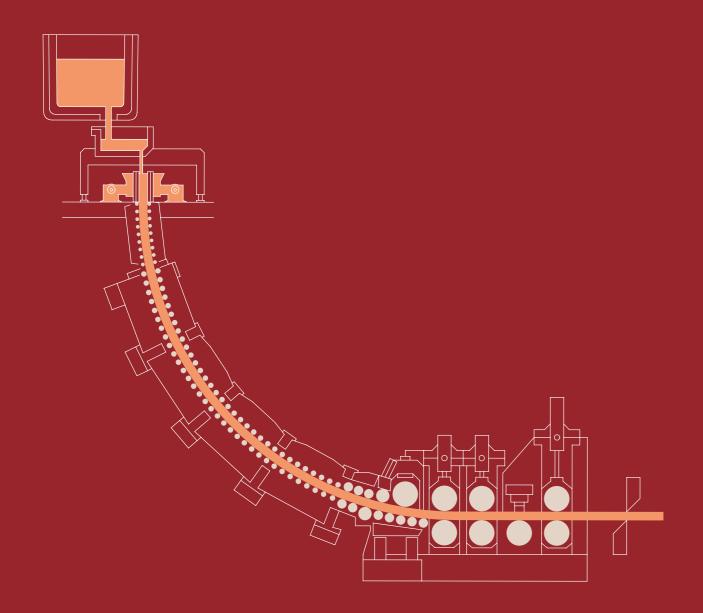


Innovative Products for Melting & Casting

The continuous casting of steel has seen major technological improvements over the past decades. This has led to considerable increase in productivity and product quality necessary to ensure survival in today's highly competitive environment. The Melting & Casting Technologies Division of cunova has been instrumental in achieving many of these process improvements.

The advances in casting technology were made possible by the development of high-performance moulds made of copper alloys. cunova was involved in these activities right from the very beginning and has conti-nued to set milestones in the development and production of copper moulds for the continuous casting and re-melting of steel and nonferrous alloys.

Our customers are manufacturers of steel and nonferrous metals, casting machine builders and maintenance companies throughout the world. The division not only serves our customers as a general contractor for the production of mould assemblies, but also as a partner in solving the many technological challenges in the field of continuous casting.



AMT® - Advanced Mould Technology

The performance requirements that have to be met by moulds and mould materials depend on the specific application and the levels of stress involved. These stress levels are mainly predetermined by the machine and casting parameters, which means that many different cast shapes are needed, depending on the type and construction of the mould. When designing a new mould, the correct profile must be chosen in order to achieve high product quality, optimal casting speeds, smooth casting operations and long service life of the moulds.

A good example of this are the requirements placed on modern mould materials for near-net-shape-casting processes which have been developed in recent years. Here, very high casting speeds are achieved and a much higher proportion of the liquid metal must solidify in order to form a sufficiently stable strand shell. The resulting extreme temperatures demand moulds with higher strength levels. At the same time, a high alternating thermal stress can occur, for example on casting rolls. This wide variety of requirements placed on moulds has to be met by highly developed materials and system expertise.

In order to be able to offer our customers futureoriented solutions for the wide variety of different casting technologies and taking into account the constantly changing requirements on moulds and mould materials, cunova is conducting research in the following fields of mould technology:

- Mould Engineering
- Mould Materials
- Mould Manufacturing
- Mould Coatings

Unlike all other manufacturers, cunova has all the key technologies for the production of high-performance continuous casting moulds under one roof. This unique combination of expertise, numerical simulation, calculation methods and long-standing experience in the field makes us a highly qualified partner in all mould related questions that arise.

AME - Advanced Mould Engineering & Design

The range of mould materials developed and produced by cunova allows appropriate selection of the optimum copper alloy for individual applications. However, in order to achieve high performance, optimum steel quality and a long service life of the moulds, further engineering work is generally necessary – particularly when casting parameters have been changed from the original concept in order to achieve higher casting outputs or produce special types of steel. This is where cunova's mould engineering service comes into play, supporting its customers in upgrading continuous casting moulds and optimising system parameters and mould constructions.

Using Finite Element Analysis (FEA) and Computational Fluid Dynamics (CFD) to calculate the mould stresses based on 3D CAD modelling allows accurate simulation of the mechanical and thermal stress factors involved in each case. Mould dimensioning, tapering and the specification of cooling conditions are based on the results of these calculations. cunova can provide detailed support on the design of new moulds. On request, cunova will also do the entire detailed engineering based on the machine builders' design drawings.

Dimensioning

When designing a mould for slab, bloom, billet or beam blank, each case must be considered individually. The main variables that play a role are the construction of the casting machine, the steel grades to be cast, the desired casting speed and the cooling conditions.

Mould Taper

The taper is one of the most important parts of the mould design, especially in case of non-adjustable moulds. When specifying the mould taper, the steel grade and the casting parameters are the main factors that must be taken into account.

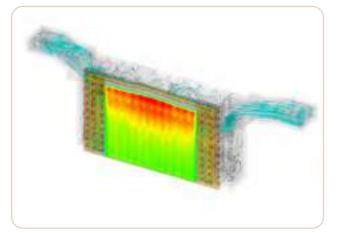
From a theoretical approach, the optimal taper of a mould can only be defined for one steel grade (due to its specific shrinkage behavior) and for one specifically defined casting condition, i.e. superheat of the liquid steel, casting speed, etc.

This means in reality, a taper can always only be a compromise that has to fit for a wider range of casting conditions. Because tailor-made parabolic tapers fulfill this task better, they are nowadays the dominating design, while tubes with linear, double or quadruple tapers are getting less in usage.

Cooling Conditions

Another important factor for designing a mould is the adjustment of cooling conditions and casting parameters in order to ensure good system productivity and product quality.

For this purpose, cunova performs CFD calculations of the water flow between cold face of the mould and the water box. In combination with the thermal load calculation of the hot face, this will give a detailed analysis of the thermal and mechanical stresses on the mould during the casting process and will support the optimisation of the design.



AFM®: FEA/CFD calculation

Advanced Smart Mould Technology for **Improved Performance**

In recent years, significant progress has been made in the development of high tech and automated steel production processes. cunova is supporting this effort with the development of our 'Advanced Smart Mould Technology'. This new technology allows for the digitalisation of key mould operating parameters that can then be optimised for improved continuous casting results.

Mould Temperature Monitoring

Monitoring the temperatures seen by the copper mould during casting is critical for process control and to understand the dynamic solidification processes during casting. Therefore, robust temperature measurement techniques are a basic requirement for the digitalisation process. cunova offers two technologies for temperature measurement and thermal monitoring:

- · The application of thermocouples in different designs and arrangements, depending on the type of casting mould.
- · The application of fibre optic measuring systems with Bragg elements that offer a substantial improvement in resolution and quality of the temperature information.

cunova has the technical know-how as well as experience to select and design these systems. Furthermore, we also have the capability to handle the installation including the very difficult deep-hole drilling (up to 2500 mm depth and 1.2 mm diameter) in both mould plates and mould tubes. Thus, we can offer a complete packaged solution for either of these systems.

Advanced Mould Organizer -**QR Mould Identification**

cunova has developed a new QR-code based system that provides mould identification and tracking. This technology is able to simplify the often-difficult task of determining the specific mould being used in the casting operation and / or maintenance shop. In the future, the QR-code will be linked to various other informations, such as mould geometry, and other product data.

Mould Sensor

A further development to broaden the cunova Advanced Smart Mould Technology is the integration of a special mould sensor that has the ability to communicate data via a 'Bluetooth' interface. This will enable easy access to key operating data such as the mould's time in service, the remaining rework potential, and other information. By using a companion software tool, data from the chip can be evaluated and archived for later analysis.



Vertical and horizontal temperature monitoring



QR Mould Identification

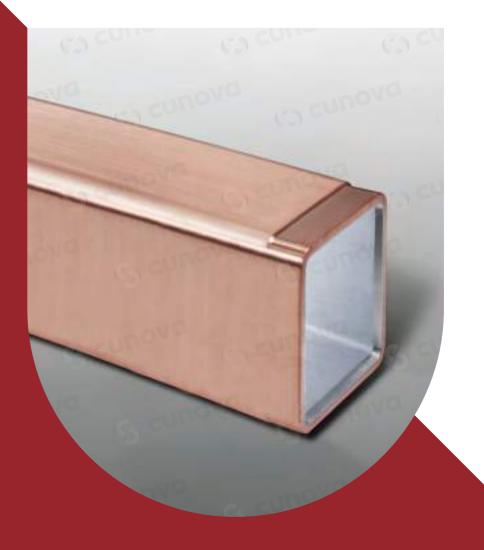


Mould Tubes for Billets, Blooms and Beam Blank

cunova develops and supplies the whole range of mould tube geometries and dimensions in use today, from small rectangular tubes right through to large-format round mould tubes. Our customers can select from various tapers and special internal geometries, such as AMT®, textured or WAVE® solutions.

cunova Manufacturing Range for Mould Tubes

| Material | • Cu-GS, CuAg-GS • ELBRODUR® G |
|----------------|--|
| Design | Square, rectangular, polygonal, round, beam blank Straight or curved Outer contour parallel Internal geometries: parallel, tapered, part-tapered, multi-tapered or parabolic CONVEX, DIAMOLD AMT® ATM WAVE® mould tubes (cunova patent) Textured mould tubes |
| Coatings | ChromeMulti-Layer-Coating |
| Sizes | Practically no limits |
| Wall thickness | Practically no limits |



Mould Tubes for Billets, Blooms and **Beam Blank**

To optimise the casting process and product quality even more, cunova offers innovative solutions that can be combined to suit the customer's specific needs for solving metallurgical or process-related technical problems.

WAVE® Tubes

The WAVE® mould has a patented design that superimposes a series of undulations onto the hot face side of the mould, causing a mirror image to be formed on the billet surface as it begins to solidify. These two surfaces will interlock and the shell will be guided through the length of the mould while restraining any movement from side-to-side.

The mould and shell are thus "coupled" together to such a degree that a more equal heat extraction, and hence uniform shell growth, occurs during this critical time. The result is improved billet shape and internal quality, as well as increased mould life.

This special design is also applicable for round sizes: Round WAVE® tubes.



WAVE® mould tube



Round WAVE® mould tube

AMT® ADVANCED MOULD TECHNOLOGY

Textured and ATM Tubes

Textured Tubes

cunova has developed a new method for controlling the heat removal in a mould tube. Using a specially developed manufacturing process, a texture can be applied to the casting surface of the mould tubes. This allows the heat transfer to be moderated in specific areas of the mould.

ATM Tubes

The ATM design is an economical way to replace bloom mould plates by a repairable mould tube design while keeping the existing waterboxes. Corner gap problems are eliminated.

The ATM design optimises the mould cooling over the entire surface area of the mould by using a uniform water gap cooling type, while reducing the internal stress in the copper due to the special low-stress bolting technology.

Furthermore the design offers more stability to the mould wall compared to conventional tube designs and is therefore favourable for large sections.



Textured mould tube



ATM: Advanced tube mould



Mould Plates for Blooms and Slabs

The design and manufacture of mould plates for bloom and slab casting machines, whether furnished with cooling slots or deep-hole drills, is a major part of cunova's product range for these applications, cunova delivers a comprehensive selection of mould materials and coatings.

cunova has developed various technology packages for the continued development of the moulds used in the casting of bloom and slab shapes. Based on a precise analysis of the cooling water flow and the load on the moulds arising from the process, an improvement in the service life can often be achieved through local optimisation of the cooling geometry.

Also completely new designs for cooling improvements were established in recent years, such as optimised-deepdrilled plates, chamfered narrow faces with special edge cooling and ASM mould plates.

ASM Mould Plates

cunova engineers have developed ASM (Advanced Slab Mould) technology to optimise the cooling of standard mould plates by converting the slot cooling design into a uniform water gap cooling type.

By using filler- or adapter plates in conjunction with the patented AFM® mounting, it is possible to reduce the working load on the moulds and to improve casting efficiency and strand quality with adjusted cooling water flow especially for curved mould plates. A significant advantage of the ASM technology is that existing moulds can be converted without requiring high investment.

Reduced Heat Dissipation

For the casting of steel grades that are prone to cracking, cunova offers materials with reduced thermal conductivity as well as solutions with textured hot faces for mould plates to achieve a reduced heat transfer in the mould.

cunova's strength in technical design together with our available materials and coatings, enables us to develop tailor-made solutions for each customer as required.



Chamfered narrow face plates

cunova Manufacturing Range for Mould Plates

| Material | • CuAg-GS/NS, ELBRODUR® H, ELBRODUR® G/GP/GP-NS • ELBRODUR® NIB |
|--------------|---|
| Plate Design | Cooling slots or cooling drills or water gap cooling type Casting surfaces straight or machined to casting radius |
| Coatings | Nickel Nickel + chrome Nickel alloy Nickel alloy + chrome Metal-Ceramic Cobalt alloy |
| Sizes | Practically no limits |



Broad face plate with improved meniscus cooling



Moulds for Near-Net-Shape-Casting

Tubes, Plates and Rolls

New continuous casting systems must guarantee high productivity, ensure good product quality and drastically reduces the specific energy consumption from raw material to finished product. These goals are being pursued with the development and introduction of nearnet-shape-casting processes. cunova played a decisive role in the development of these technologies by developing materials, optimising geometry and cooling and adapting the coating for the moulds. By engineering new mould concepts such as the Advanced Funnel Mould (AFM®) and the Advanced Beam Blank Mould (ABBM), cunova continues to set milestones in the development of moulds for near-net-shape-casting technology.

Moulds for Beam Blank Casting

A multi-part plate mould or a mould tube can be chosen for beam blank casting. Plate constructions give a greater degree of freedom when specifying the mould taper and coating, whereas tubes make it possible to use casting oils. Repair techniques for both types of moulds are available at cunova.

ABBM - Advanced Beam Blank Mould

The cunova Advanced Beam Blank Mould is an innovative development in mould technology for beam blanks. The combination of a thin-walled copper plate with a water gap cooling type and a support plate permits the separation of functions in this mould type. For the first time, it is now possible to use thin-walled copper plates for optimised heat dissipation without losing any of the maintenance-friendly qualities of plate construction.

Mould Plates for Thin Slab Casting

The casting of thin slabs is the most common method of near-net-shape technology used today. The mould takes on particular importance for the performance of the system. Due to the changed surface / volume ratio in this method, about 50 % of the slab thickness solidifies in the mould, compared with 10 % in conventional slabs. This means that large amounts of heat have to be removed by the mould and the copper is subject to extreme thermal stresses. cunova's development of new materials and the production are decisive advantages that can be utilised here. Today, cunova manufactures CSP, ISP, ESP, fTSC and DUE mould plates for thin slab casting.

AFM® - Advanced Funnel Mould

cunova has engineered the innovative Advanced Funnel Mould (AFM®), which consists of a thin-walled copper plate and an adapter plate.

The thin copper plate allows high heat transfer rates, which is a basic requirement for improved casting efficiency. In addition, the thickness of the mould plate is adapted to the specfic heat load in different areas of the mould. Combined with the water gap cooling design this results in homogeneous surface temperatures for uniform melting of the casting flux, and thus improved slab surface quality.

A patented connection to the adapter plate allows a controlled heat expansion of the copper plate during casting, in order to reduce the operating stresses in the copper plates.

The adapter plate makes it possible to fit the mould to an existing water box without additional changes.

ATSM - Advanced Thin Slab Mould

The ATSM Mould is cunova's newest design upgrade for thin slab caster. Like the AFM®- and ABBM-mould the ATSM-mould is compatible with existing water boxes. It consists of an improved copper plate design (Patent Applied) with broad cooling fields for a homogenous cooling and an innovative anti-bulging system (Patent Applied) to counteract meniscus bulging.

As additional feature for easy maintenance the ATSM design uses a few swivelling filler plates instead of numerous filler bars as used at the standard designs.

With this feature the ATSM offers maintenance-friendly access to the water-cooled copper surfaces for easy inspection and cleaning.



ABBM - Advanced beam blank mould



Mould plates for thin slab casting



AFM® - Advanced funnel mould



ATSM plate





Moulds for Near-Net-Shape-Casting

Moulds for thin Strip Casting

As early as 1891, Sir Henry Bessemer drafted the principle of a casting machine in which the molten steel was supposed to solidify directly into steel strips between two casting rolls. Just over a hundred years later, his idea has become reality.

As a result of the unusually high surface/volume fractions that prevail in strip casting, great amounts of heat have to be conducted away by the casting rolls. cunova can meet the extremely high demands on materials and the manufacturing precision required for all the various strip casting machines in use around the world. Customerspecific adaptations of the material

characteristics to the cooling conditions and to the load situation are an important key to the successful development of the technology.

Since cunova controls all stages along the entire process chain, it is possible for us to deliver specific engineered solutions for each individual customer and hence support start-up and production process.

cunova manufactures according to OEM drawing and specification, including steel shafts, if requested for "ready to use" state.

Manufacturing Range for Near-Net-Shape Moulds

| Type of Mould | Form | Materials | Design | Size | Coatings |
|---------------|------------------|---|---|--------------------------|--|
| Thin Slab | Plates | CuAg-NS ELBRODUR® H ELBRODUR® G/GP/ GP-NS ELBRODUR® NIB | With cooling slots or drilled cooling channels Casting surfaces with special contours for casting thin slabs Straight or machined in accordance with casting radius CSP, ISP, ESP, fTSC, DUE, AFM®, ATSM | Practically no limits | Nickel Nickel alloy Metal- Ceramic Cobalt alloy |
| Beam Blank | Tubes | CuAg-GS ELBRODUR® G | - External contour parallel - Internal geometries: parallel, part-tapered, multi-tapered, or parabolic, and with special internal contours for casting beam blanks with additional cooling channels | Practically no limits | Chrome |
| | Plates | CuAg-GS/NS ELBRODUR® G/GP/ GP-NS | - With cooling slots or drilled cooling channels ABBM | Practically no limits | Nickel Nickel + chrome Nickel alloy + chrome Cobalt alloy + Cr |
| Thin Strip | Casting rolls | ELBRODUR® G/GP ELBRODUR® NIB ELBRODUR® B 95/ B 95S | – Cooling system in the shape of slots or drilled channels, depending on overall design | Practically no limits | Upon request |

AMM – Advanced Mould Materials

Material sciences and the development of copper alloy systems have for many years represented an important area for cunova as the leading manufacturer of copper products. A major part of cunova's efforts in these fields is dedicated to the development of copper alloy systems for continuous casting moulds. Therefore, depending on the application and the range of properties required, the mould material can be adjusted using specially tailored alloys.

Cu-GS

DHP copper was developed as a standard material for mould tubes under normal service conditions at temperatures in the meniscus area of up to about 300 °C. The material displays excellent heat and creep resistance at high temperatures and its workability is good.

CuAg-GS/NS

Copper-silver alloys (CuAg) are used in applications in which higher thermal stresses and wall temperatures occur. CuAg alloys have a higher thermal conductivity, which means that the temperatures in the mould can be kept on lower levels. In addition, they have higher temperature resistance to softening than DHP-Cu.

ELBRODUR® H

ELBRODUR® H is a newly developed advanced material based on approved ELBRODUR® G alloy. This material is designed to bridge the gap between the highly conductive copper silver alloys and the creep resisting, precipitation hardened alloys like ELBRODUR® G. The material was developed for the application with netshape-casting operations.

ELBRODUR® G

ELBRODUR® G is an age hardenable CuCrZr alloy which has excellent mechanical properties, both at room and higher temperatures. High heat conductivity, a very high softening temperature, high creep resistance and high resistance to alternating thermal stresses are exceptional properties that set this alloy apart from the copper alloys previously presented. The good combination of properties achieved in this material is made possible by the use of alloying elements and a special thermo-mechanical treatment (see Fig. 1 – 4).

ELBRODUR® GP

ELBRODUR® GP is an advanced material developed on the basis of the approved ELBRODUR® G. It has been possible to further improve this material's properties through careful tuning of the chemistry and process control during manufacture.

ELBRODUR® GP-NS

ELBRODUR® GP-NS is an advanced material developed on the basis of the approved ELBRODUR® GP, but with a higher strength level. It was developed for near-netshape-casting applications, such as beam blank and thin slab moulds.

ELBRODUR® B 95

This is a high-alloyed age hardenable CuCoBe based material which has medium conductivity, along with very good elevated temperature strength. This material is suitable for very special applications requiring reduced cooling, such as casting rolls.

ELBRODUR® NIB

This is a material based on CuNiBe. It has been developed specifically for use in moulds for near-net-shapecasting and other moulds that need to withstand particularly high stresses.

Its outstanding characteristics are high strength along with medium conductivity. Importantly, it has a special resistance to cracking when exposed to thermal stresses caused by large temperature fluctuations in the mould wall.



Different mould tube designs made of different copper alloys.

AMM – Advanced Mould Materials

Performance Requirements for Copper Materials

Mould Function, Type of Exposure Handling; assembly/disassembly Transfer of superheat and heat loss of solidification High wall temperatures Mechanical stresses at high temperatures Heavily fluctuating thermal stresses

| Properties re | quired |
|---|----------------|
| High basic hardness a | nd strength |
| High thermal cond | uctivity |
| Retention of high strength operating temper | |
| High resistance to | creep |
| High resistance to fatigue | e and cracking |
| High hardness and resist | ance to wear |
| Reduced electrical co | onductivity |

Figure 1

Recrystallisation/softening behaviour of cunova mould materials versus standard copper (ETP Cu)



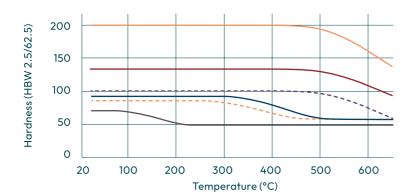


Figure 2

Creep characteristics of plate crucible materials (temperature 200 °C/392 °F, stress 150 MPa)



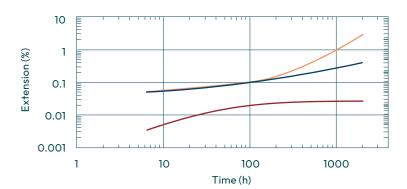


Figure 3

Hardness and electrical conductivity of cunova mould materials



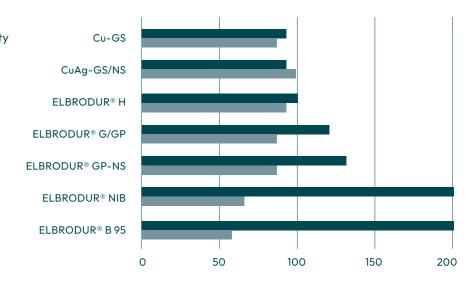
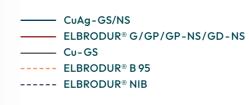
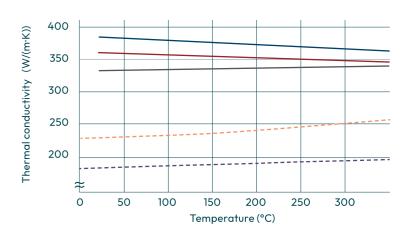


Figure 4

Effect of temperature on thermal conductivity of cunova mould materials





AMM – Advanced Mould Materials

cunova Materials for Mould Tubes

| Material Properties* | Temperature | Units | Cu-GS | CuAg-GS | ELBRODUR° G |
|---------------------------------------|-------------|-------|--------|---------|-------------|
| Chemical Composition (without Copper) | | % | 0.03 P | 0.09 Ag | 0.65 Cr |
| (willion Copper) | | (3) | cunos | 0.006 P | 0.1 Zr |
| | | | | | |

| Physical Properties | °C | °F | | | | |
|----------------------------------|--------|--------|---------|--------|-------|-------|
| Electrical Conductivity | 20 | 68 | S·m/mm² | 48 | 55 | 50 |
| | | EUIL | % IACS | 83 | 95 | 86 |
| Thermal Conductivity | 20 | 68 | W/(m·K) | 340 | 377 | 355 |
| Coefficient of thermal Expansion | 20-300 | 68-572 | 10-6/K | 97.7 | 17.7 | 18 |
| Recrystallisation Temperature | - | - | °C | 350 | 370 | (800) |
| Softening Temperature** | | SOIL | °C (\$) | COLICE | ري حل | 580 |
| Modulus of Elasticity | 20 | 68 | 10³ MPa | 120 | 125 | 128 |

Units: 1 MPa=1 N/mm²=0.102 kgf/mm²=0.145 ksi; 1 W/(m·K)=2.388 · 10³ cal/(cm·s·°C)

| Material Properties* | Tempe | erature | Units | Cu-GS | CuAg-GS | ELBRODUR° G |
|--------------------------------------|-------|---------|--------|-------|---------|-------------|
| Mechanical Properties | °C | °F | wa | ~10 | | avd. |
| 0.2 % Proof Stress R _{p0.2} | 20 | 68 | MPa | 290 | 290 | 360 |
| | 200 | 392 | | 260 | 260 | 335 |
| | 350 | 662 | - un | (215) | (215) | 295 |
| | 500 | 932 | C) co. | (20) | (20) | (185) |
| Tensile Strength R _m | 20 | 68 | MPa | 310 | 310 | 430 |
| | 200 | 392 | (3) | 265 | 265 | 400 |
| | 350 | 662 | | (220) | (220) | 340 |
| | 500 | 932 | aun (| (80) | (80) | (210) |
| Elongation A ₅ | 20 | 68 | % | 16 | 16 | 19 |
| | 200 | 392 | va | 14 | 14 | 18 |
| | 350 | 662 | (3) | (12) | (12) | 19 |
| | 500 | 932 | | (70) | (70) | (20) |
| Hardness HBW 2.5/62.5 | 20 | 68 | CA CUN | 95 | 95 0 0 | 130 |

Units: 1 MPa=1 N/mm²=0.102 kgf/mm²=0.145 ksi; 1 W/(m·K)=2.388 · 10³ cal/(cm·s·°C)

^{*} Values may change with varying thermal and mechanical treatment due to geometry and manufacturing procedure

^{**} Measurement according to DIN ISO 5182

⁽⁾ Values may change due to restricted reproducibility of measurement

 $^{^{*}}$ Values may change with varying thermal and mechanical treatment due to geometry and manufacturing procedure

^{**} Measurement according to DIN ISO 5182

⁽⁾ Values may change due to restricted reproducibility of measurement

AMM – Advanced Mould Materials

cunova Materials for Mould Plates, Block Moulds and Casting Rolls

| Material Proper- ties* | Tempe- rature | Units | CuAG- GS | CuAG- NS | ELBRO- DUR° H | ELBRO- DUR° G/GP | ELBRO- DUR° GP-NS | ELBRO- DUR° B95 | ELBRO- DUR° B95S | ELBRO- DUR° NIB |
|------------------------------------|------------------|-------|-------------|-------------|---------------------|------------------------|-------------------------|-----------------------|------------------------|-----------------------|
| Chemical | ova | % | 0.09 Ag | 0.1 Ag | 0.1 Zr | 0.65 Cr | 0.65 Cr | 1.0 Co | 1.4 Co | 1.5 Ni |
| Composition (without Copper) | | (3) | 0.006 P | 0.004 P | Ag | 0.1 Zr | 0.1 Zr | 0.1 Be | 0.3 Be | 0.2 Be |

| Physical Properties | °C | °F | | | | | | | | | |
|--|------------|------------|---------------------|------|----------|-------|-------|-------|-------|-------|-------|
| Electrical Conducti- | 20 | 68 | S·m/mm² | 54 | 57 | 54 | 48 | 49 | 35 | 31 | 40 |
| vity | | | % IACS | 93 | 98 | 93 | 83 | 84 | 60 | 54 | 69 |
| Thermal Conducti- vity | 20 | 68 | W/(m·K) | 377 | 385 | 370 | 350 | 350 | 240 | 220 | 290 |
| Coefficient of thermal Expansion | 20- 300 | 68- 572 | 10 ⁻⁶ /K | 17.7 | 17.7 | 17.7 | 18 | 18 | 18 | 18 | 18 |
| Recrystalli- sation Tempera- ture | - | - | °c | 370 | 350 | (700) | (800) | (800) | (800) | (800) | (800) |
| Softening Tempera- ture** | Vo | 7 - 0 | °C | | va va | 530 | 580 | 580 | 590 | 590 | 590 |
| Modulus of Elasticity | 20 | 68 | 10 ³ MPa | 125 | 125 | 125 | 128 | 128 | 128 | 128 | 128 |

Units: 1 MPa=1 N/mm² = 0.102 kgf/mm² = 0.145 ksi; 1 W / (m·K) = $2.388 \cdot 10^3$ cal/(cm·s·°C)

| Material Proper- ties* | | npe- ure | Units | CuAG- GS | CuAG- NS | ELBRO- DUR° H | ELBRO- DUR° G/GP | ELBRO- DUR° GP-NS | ELBRO- DUR° B95 | ELBRO- DUR° B95S | ELBRO- DUR° NIB |
|------------------------------|-----|-------------|------------|-------------|-------------|---------------------|------------------------|-------------------------|-----------------------|------------------------|-----------------------|
| Mechanical Properties | ္င | °F | 63 | cuno | | | uno) | | | NOU | a |
| 0.2 % Proof | 20 | 68 | | 275 | 285 | 270 | 285/330 | 370 | 490 | 610 | 510 |
| Stress R _{p 0.2} | 200 | 392 | MPa | 245 | 255 | 240 | 260/290 | 330 | 450 | 580 | 500 |
| | 350 | 662 | MPd | (200) | (200) | 230 | 230/255 | 300 | 430 | 540 | 470 |
| | 500 | 932 | | (20) | (20) | (190) | (200/220) | (245) | (400) | (450) | (420) |
| Tensile | 20 | 68 | 150 | 280 | 290 | 310 | 410/420 | 430 | 630 | 720 | 630 |
| Strength | 200 | 392 | MPa | 250 | 250 | 265 | 350/365 | 370 | 570 | 670 | 570 |
| R _m | 350 | 662 | MFG | (210) | (210) | 240 | 295/310 | 325 | 500 | 600 | 510 |
| | 500 | 932 | cung | (80) | (80) | (195) | (230/250) | (255) | (440) | (500) | (430) |
| Elongation | 20 | 68 | | 16 | 17 | 21 | 25/22 | 19 | 13 | 10 | 12 |
| A ₅ | 200 | 392 | | 14 | 15 | 19 | 24/20 | 16 | 11 | 3V | 10 |
| | 350 | 662 | % | (12) | (12) | 17 | 22/19 | 16 | (5) | (3) | (4) |
| | 500 | 932 | <i>7</i> 6 | (70) | (70) | (16) | (22/19) | (16) | (3) | (2) | (3) |
| Hardness HBW 2.5/62.5 | 20 | 68 | cuna | 90 | 90 | 100 | 120/130 | 135 | 200 | 235 | 200 |

Units: 1 MPa=1 N/mm² = 0.102 kgf/mm² = 0.145 ksi; 1 W / (m · K) = $2.388 \cdot 10^3$ cal/(cm·s·°C)

 $^{^{*}}$ Values may change with varying thermal and mechanical treatment due to geometry and manufacturing procedure

^{**} Measurement according to DIN ISO 5182

⁽⁾ Values may change due to restricted reproducibility of measurement

¹⁾ Hardness HBW: 2.5 /187.5 for ELBRODUR® B 95 and ELBRODUR® NIB

^{*} Values may change with varying thermal and mechanical treatment due to geometry and manufacturing procedure

^{**} Measurement according to DIN ISO 5182

⁽⁾ Values may change due to restricted reproducibility of measurement

¹⁾ Hardness HBW: 2.5 /187.5 for ELBRODUR® B 95 and ELBRODUR® NIB



AMC® - Advanced Mould Coatings

Nowadays the majority of all copper moulds around the world are hot face coated - to either protect the copper against abrasive wear or diffusion of harmful elements or – to protect the surface quality of the cast product against copper pick-up (star cracks). cunova has developed different advanced mould coatings to serve these special needs.

Copper materials have a relatively low hardness and thus low resistance to abrasive wear. For this reason, a high degree of wear can occur, mainly in the lower part of the mould. The main object of coating mould tubes and plates is to increase the service life of the mould, as well as an improvement in the product quality.

cunova has come up with future-oriented solutions by further developing and by using new coatings and coating-systems. New wear-protection layers and coating techniques are also being investigated in our laboratories.

Coating of Mould Tubes

The small size billet moulds, are particularly susceptible to wear. The hard chrome coating AMC-HC 90 on the inside mould surfaces provides effective anti-wear protection which results in a substantial gain in mould lifetime.

AMC-HN50

The AMC-HN50 coating is the latest development belonging to the cunovas mould coating family. The HN-50 coating is based on a electrolytic nickel and its be tailor made to the application whether it for mould tubes or plates. Beside higher hardness and wear resistance it is superior in terms resistance to chemical induced wear.

AMC®-ML Multi-Layer

In casting operations, mould tubes are exposed to an extreme varity of operational loads. In addition to a high thermal and high abrasive load, the steel melt often also introduces tramp elements into the process which cause a chemically induced damage. Such tramp elements like zinc or sulphur often originate from the steel scrap.

The formation of cracks and as a result a spalling of the coating in the meniscus level are typical damage patterns which necessitates a replacement of the mould tube.

As a countermeasure cunova has developed the multi layer AMC-ML coating to provide effective protection of the mould tube against the combined chemical, thermal and mechanical loads.

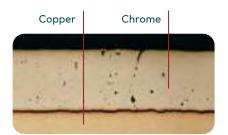


AMC® - Advanced Mould Coatings

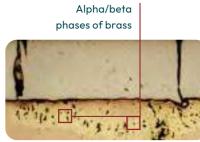
Coating damage from Zinc

Zinc from the steel melt can initiate a specific failure mechanism in connection with chrome coatings. Vaporising zinc mainly from scrap makes its way to the copper surface by diffusing into the micro cracks which are always present in hard chrome. High mould temperatures encourage the diffusion, so that the problem mainly occurs in the mould meniscus area,

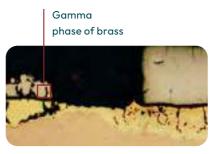
especially if cooling conditions are unfavourable. The copper reacts with the zinc forming brittle, and "bulky", intermetallic phases of brass which result is premature chrome chipping.



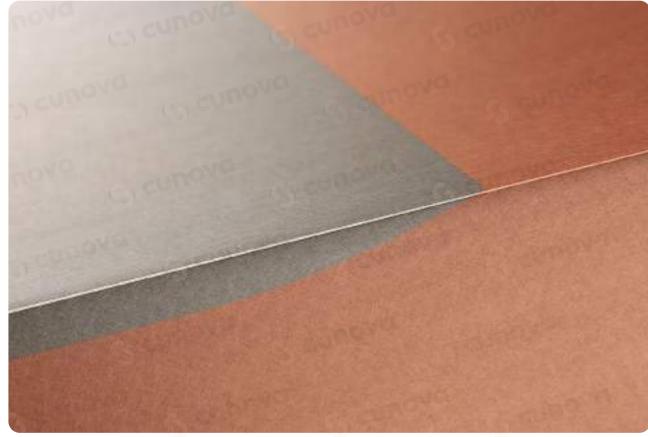
Original chrome coating (cross section)



First damage stage



Final failure stage: chrome layer flakes off



Step coated narrow face copper plate

Coating of Mould Plates

When it comes to coatings for mould plates, a distinction has to be drawn between

- · coatings for metallurgical protection to improve the surface quality of the cast strand (e.g. prevention of star cracks), and
- · anti-wear coatings to improve resistance to abrasion.

Depending on the distinction and the overall conditions at the plant the casting surfaces of the mould plates are either full-face coated or only partially with nickel, nickel alloys or special ceramic coatings. Also multi-layer coatings are possible.

Metallurgical necessary Coating

When casting certain steel grades the surface quality of the cast strand can become impaired by copper particles picked up from the mould wall (especially in the lower part of a mould) which can lead to the development of star cracks. To avoid this defect, the mould plates of slab casters used for the production of these sensitive steel grades are protected with a nickel or nickel-alloy coating.

Anti-wear Coatings

Considering the lower thermal conductivity of coating materials a decision for the right coating geometry has to be made.

As a result of the associated reduction in mould heat transfer, and because of the resultant higher wall temperatures which affect nickel adherence to the copper, thick nickel coatings have a major impact on the operational handling and relevant casting parameters. This puts definite limits on the maximum allowable nickel thickness in the meniscus area.

The table shows the effect of nickel plating thickness on heat transfer and wall temperature From the point of view of caster operation, a reduction of approx. 3.8 % in heat transfer with 3 mm nickel on the copper is not significant, but the accompanying 45° C increase in wall temperature causes considerable stresses in the nickel due to the difference in coefficients of thermal expansion of the two metals.

Due to that, hairline cracks may develop in the nickel at the mould meniscus and can propagate into the copper. For this reason undue coating thickness should be avoided, especially in the meniscus area.

Nickel alloys, like cunova's AMC-HN 40 or AMC-HWR are an interesting alternative to pure nickel layers. As a result of their greater hardness, they have good anti-wear properties with slightly lower thermal conductivity.

For the reasons outlined above, tapered nickel (alloy) coatings that are approx. 1.0 mm thick at the top and approximately 3.0 mm thick at the bottom end, or 2 – 6 mm thick partial coatings on the lower half of mould plates, represent optimal solutions with respect to both metallurgical and cost requirements.

AMC® - Advanced Mould Coatings

Effect of Nickel Thickness on Heat Transfer and Wall Temperature

Calculation based on constant coefficients of heat transfer; heat flux approx. 1.8 MW/m².

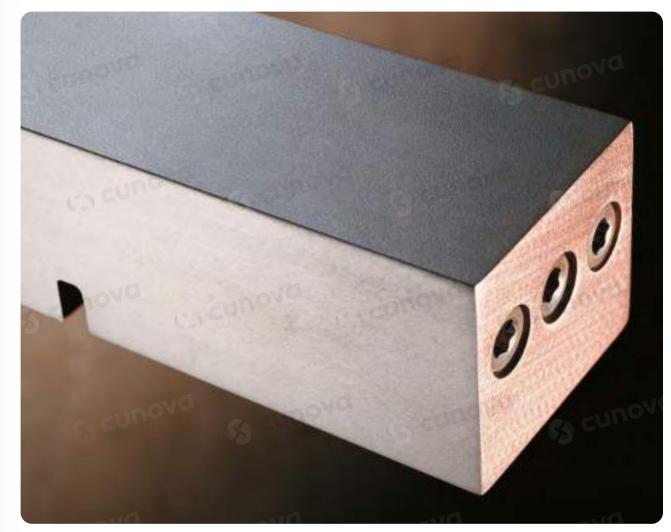
| Material: CuAg (DPS-Cu) | Ni coating mm | ∆T wall °C | Δ heat transfer % |
|----------------------------|------------------|---------------|--------------------------|
| - CUNOVO | 0.7 | +11 | -0.9 |
| Wall thickness: | 1 | +15 | -1.3 |
| 35 mm | 2 | +30 | - 2.6 |
| | 3 2000 | +45 | - 3.8 |



Center divider with coating on hot face

For adjustable slab and bloom moulds, friction between the surfaces of the wide-face coppers and the edges of the narrow face coppers leads to wear and the localised development of deep scores and scratches.

Here, the rate of wear can be reduced considerably by coating the edges of the adjustable narrow face plates, which slide on the inside (hot face) of the wide-face coppers, with a material that has greater hardness.



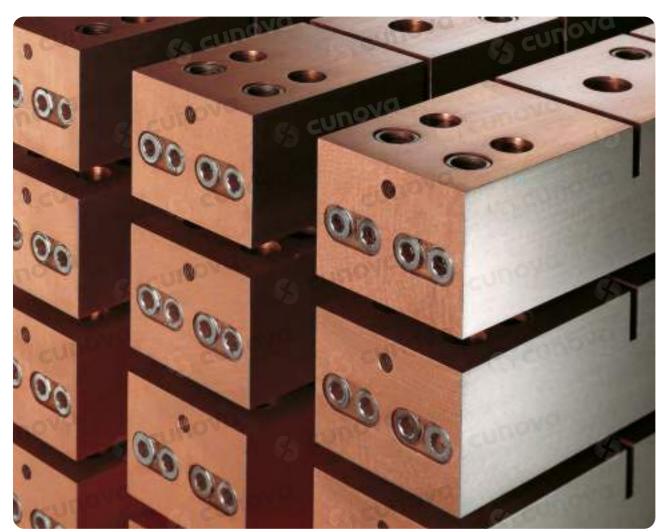
Deep-drilled narrow face plate for thin slab mould with coating on hot face and edges

AMC® - Advanced Mould Coatings

Beside the nickel and nickel-alloy coatings, cunova can also supply metal-ceramic coatings (AMC-HF). The high hardness of such coatings makes it possible to achieve considerable improvements in the lifetime, especially of narrow face plates.

It can be seen that very complex interrelationships have to be taken into account when selecting a suitable coating and layer thickness. Recommendations can therefore only ever be made in relation to specific system and casting parameters. Close consultation between the system operator and the mould supplier is necessary to ensure that the appropriate coating systems are selected.

The selection of coating may furthermore depend on what possibilities exist in terms of mould maintenance and available re-coating services.



Deep-drilled narrow face plates for thin slab mould with coating on hot face and edges



AMC® - Advanced Mould Coatings

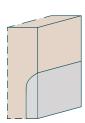
The thermal spray coating AMC - HF 120, which feature different sets of properties, make it possible to achieve further reductions in mould wear and/or wear at the edges of narrow face mould plates. Its extremely low abrasive wear makes AMC - HF 120 the preferred coating for the hot faces. Tests done with narrow face plates have demonstrated its excellent in-service performance. In some cases it may be impossible for the technical potential of spray coatings to be fully exploited.

The facial wear may be extremely low, but the handling of mould plates with these coatings requires much greater care and attention in order to avoid local damage. It is in the nature of very hard (coating) materials to possess

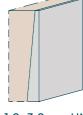
lower ductility than electroplated nickel deposits, and this is where that typical property makes itself felt. Thermal conductivity decreases as hardness increases, and spray coatings do feature low conductivity values. But this remains without any negative effect, even in the case of full-surface coatings, since deposits a few tenths of a millimetre thick are not acting as a major heat flux barrier.

On the basis of initial test runs under normal shop-floor conditions mould life can be expected to increase by a typical factor of 3 to 6, the reference basis being hot face coatings of AMC-HN 20 and AMC-HN 40 which do of course last much longer already than plates with no coating at all.

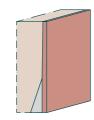
Coatings for Plates



2.0-6.0 mm HN 20 or 2.0-3.0 mm HN 40/HWR



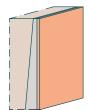
1.0-3.0 mm HN 20 or 1.0-2.0 mm HN 40/HWR



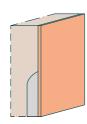
 $0.3 \, \text{mm} + 3 \, \text{mm}$ HN 20/HN 40/HWR



1.0 - 3.0 mm HN 50



1.0-3.0 mm HN 20/40/ HWR + 0.025-0.05 mm HC 90



2.0-6.0 mm HN 20+ 0.025-0.05 mm HC 90

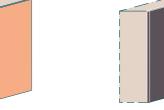
0.1 mm ML (Multi-Layer)



0.1-0.6 mm HF 120

Coatings for Tubes



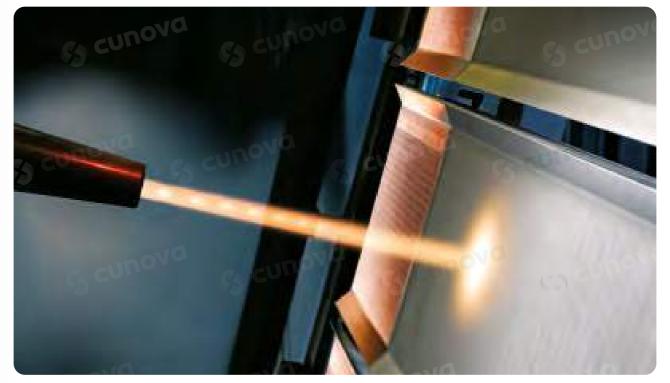


0.1 mm HN 50

AMC® - Advanced Mould Coatings | Hardness, Thermal Conductivity and Thickness Range

| Material | Hardness* HV | Thermal conductivity W/(m·K) | Thickness range mm |
|---------------------|-----------------|---------------------------------|-----------------------|
| MC®-HN 20 | 220 | 90 | 2-6 |
| AMC®-HWR | 240 | 80 | 2-3 |
| AMC®-HN 40 | 400 | 80 | 2-3 |
| AMC®-HN 50 | 500 | 80 | 2-3 |
| AMC®-HF 120 | 1200 | 30 | 0.1-0.6 |
| AMC®-HC 90 | 900 | 70 | 0.05-0.12 |
| AMC®-ML Multi-Layer | 220/900 | 90/70 | >0.5 |

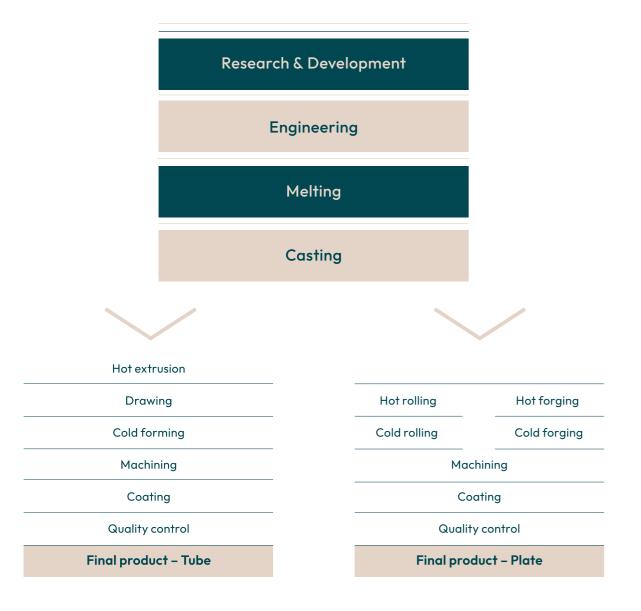
^{*} Data may fluctuate



Thermal spray coating on a chamfered narrow face.

0.08 mm - 0.12 mm HC 90

Advanced Mould Manufacturing

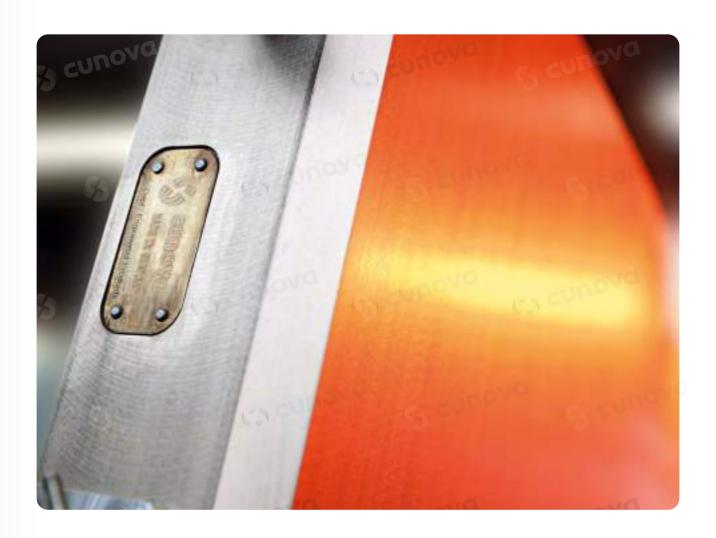


AMT® ADVANCED MOULD TECHNOLOGY

Quality Assurance

The use of high-quality products is absolutely imperative for the safe operation of continuous casting facilities. In order to ensure this, cunova has all production and business processes certified to DIN ISO 9001.

These comprehensive capabilities give cunova the start-tofinish control needed to pursue its business philosophy on all levels involved and through all stages of production.



cunova Mould Service Worldwide



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AMT® ADVANCED MOULD TECHNOLOGY

Service for Maintenance and Re-Coating

Mould Assemblies

From the smallest size billet mould to remotely adjustable slab moulds – cunova builds and assembles all types of casting moulds complete with their complex drive and control systems.

Here, too, the uncompromising quality standards of cunova are ensured through in-process quality control at all stages of a project, no matter whether it is a one-off job or the manufacture and assembly of a whole series of moulds. These services for maintenance and re-coating are for customer's requirements on a worldwide basis.

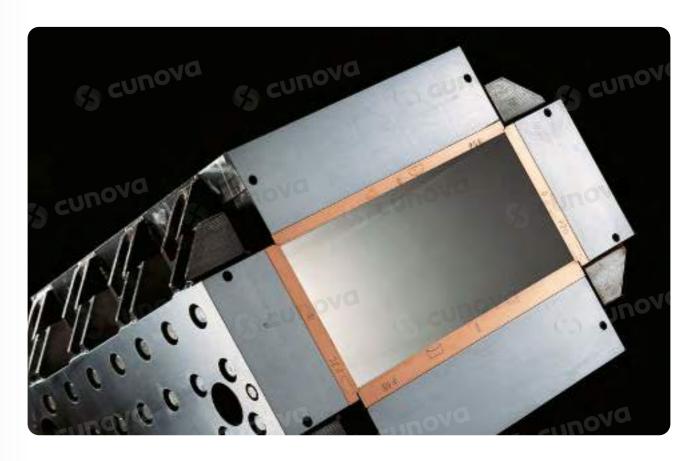
Repair of Mould Tubes

As a matter of basic principle, mould tubes are designed as expendable items. Yet, in certain cases it may be economically worthwhile for a client to have his largesection mould tubes reworked.

Repair of Mould Plates

cunova's maintenance and repair services for mould plates include the proper remachining as well as repair of stud-welded moulds and possible re-coating of the copper, plus a complete overhaul of the entire mould assembly, if needed.

In the case of a complete mould overhaul, the mould will be dismantled and all its mechanical and supporting parts will be inspected and, if necessary, renewed. Like cunova's newly built moulds, the reassembled unit complete with the remachined copper – or with new copper, if necessary - will undergo a complete operational check.



Developments on Mould Tubes

1960

Manufacture of the first copper mould tubes for continuous casting of steel Size range 80-120 mm





1963-1965

Development of a special manufacturing process to ensure a reproducible qualityregarding

- high dimensional stability
- close tolerances
- Broadened size range
- All shapes



0.06 - 0.08 mm Cr

0.10 - 0.12 mm Cr

Curved Inside tapered

1965/66

Development and use of Cr-plated mould tubes



From 1980

Improvement of mould tube geometry to meet high-standard market requirements

- set up individual taper
- modification of corner radii
- modification of wall thicknesses
- closer tolerances



1982

Supply of first mould tubes with beam blank moulds



Curved tapered Cr-plated

1986/95

Supply of world's largest mould tubes Square Round





360 x 320 mm ø 600 mm





1994/95

Supply of mould tubes with special geometries for high speed billet casting

- CCT® Mould
- cunova AMT Mould
- DIAMOLD

Gun-drilled beam blank moulds



Development of improved chrome coating

1998/2001/2002

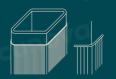


2006

Development of the cunova homogenous cooling mould tubes



Development of the cunova AHE advanced high efficency mould tube



Development of the cunova ATM advanced mould tube



Development of the cunova textured mould tube



2012

Development of the cunova WAVE® mould tube



2018

Development of the cunova round WAVE® mould tube



2023

Development of the cunova CV Cooling Design



AMT® ADVANCED MOULD TECHNOLOGY

Developments on Mould Plates

1964

Start of manufacture and reconditioning of complete non-adjustable slab moulds



Size 200 x 1700 mm

1966/70

Development and use of the special alloys of CuAg and ELBRODUR® G

Extreme dimensional stability i.e. resistance to deformations

- · high thermal conductivity
- · excellent high temperature strength
- high creep resistance

1968

Supply of the first beam blank moulds 2-piece design



Size 560 x 265/100 mm

1969/70

Supply of adjustable slab moulds



1975

Continued development of electrodeposited nickel coatings + ceramic coatings





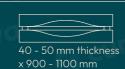
1986 Supply of the first beam blank moulds, 4-piece design



Size 685 x 225/50 mm

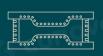
1988

Supply of the first thin slab moulds



1990

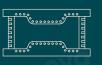
Supply of wide flange beam blank moulds 4-piece design



Size 500 x 410/123 mm

1994

Supply of wide flange beam blank moulds 4-piece design



Gun-drilled funnel mould with optimised cooling design by cunova



Size 1120 x 500/130 mm

2003

Development of the cunova AFM® mould



2006

AFM® mould running in industrial-scale production



2007

Development of the cunova ABBM beam blank mould



2009

ASM advanced slab mould



Development of the ESP mould



ELBRODUR® GP-NS

– fatigue behavior

- creep strength

2012/2013

Development and use of the cunova special alloy **ELBRODUR® GD-NS**



2017

Development of the cunova ATSM mould



2019

Supply of mould with fibre optical systems











Further information on AMT® Advanced Mould Technology:

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